



Measure of maturity of the concrete structure

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Article information

DOI:

<http://dx.doi.org/10.21041/ra.v6i3.149>

Article received on May 30, 2016, reviewed under publishing policies of ALCONPAT journal and accepted on August 16, 2016. Any discussion, including authors reply, will be published on the third number of 2017 if received before closing the second number of 2017.

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ALCONPAT Journal, year 6, No. 3, September-December 2016, is a quarterly publication of the Latinamerican Association of quality control, pathology and recovery of construction- International, A.C.; Km. 6, Antigua carretera a Progreso, Mérida, Yucatán, C.P. 97310, Tel.5219997385893, alconpat_int@gmail.com, Website: www.alconpat.org.

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ABSTRACT

In this paper we determine the degree of maturity in situ concrete structure. To do this, temperatures are measured in the concrete foundations of a structure, from the first hours of hydration, to 28 days, with a device developed at the Faculty. Simultaneously testing compressive strength are performed establishing the relationship with temperature, with expressions Nurse-Saul and Arrhenius. The results allowed to determine the maturity curve of the studied concrete and establish the degree of maturity in each of the different parts of the structure.

The use of this methodology allows to control the entire concrete received, its homogeneity and to monitor resistance in real time.

Keywords: maturity; concrete; temperature; resistance.

RESUMEN

En este trabajo realizamos la determinación del grado de madurez del hormigón in situ en una estructura. Para ello, se miden las temperaturas en las bases de hormigón de una estructura, desde las primeras horas de la hidratación, hasta los 28 días, con un equipo desarrollado en la Facultad. Simultáneamente se realizan ensayos de resistencia a la compresión estableciendo la relación con las temperaturas, con las expresiones de Nurse-Saul y Arrhenius. Los resultados permitieron determinar la curva de madurez del hormigón estudiado y establecer el grado de madurez en cada una de las partes diferenciadas de la estructura.

El uso de esta metodología permite controlar la totalidad del hormigón recibido, su homogeneidad y monitorear su resistencia en tiempo real.

Palabras claves: madurez; hormigón; temperatura; resistencia.

RESUMO

Neste trabalho, determinar o grau de maturidade na estrutura de concreto situ. Para fazer isso, as temperaturas são medidas nas fundações de betão de uma estrutura, desde as primeiras horas de hidratação, a 28 dias, com um dispositivo desenvolvido na Faculdade. Simultaneamente testar resistência à compressão são realizados estabelecer a relação com a temperatura, com expressões Nurse-Saul e Arrhenius. Os resultados obtidos permitem determinar a curva do betão estudada maturidade e estabelecer o grau de maturação em cada uma das diferentes partes da estrutura.

A utilização desta metodologia permite controlar todo o betão recebido, a sua homogeneidade e monitorar a resistência em tempo real.

Palavras-chave: maturidade; betão; temperatura; resistência.

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1. INTRODUCTION

The maturity method provides a simple and useful middle to estimate the strength gain of concrete in early ages (generally less than 14 days).

It should be mentioned that it is necessary to have the maturity curve of the dosage to be used, because the curve is typical of all materials used.

This method recognizes the combined effect of time and temperature, providing a basis for estimating the concrete strength development of "in situ" by controlling the temperature and time (Peter C. Taylor, Steven H. Kosmatka, Gerald F. Voigt, et al, 2007).

The effects of time and temperature in the increased concrete strength are quantified by a function of maturity, that is indicative of the level of resistance developed by the concrete. The two functions of maturity used for this purpose are for Nurse-Saul and Arrhenius (325.11R ACI-01, 2001).

The equation of Nurse-Saul, developed in the 50s and the most widely accepted to measure maturity, is the accumulated product of the time and temperature, equation 1.

$$M(t) = \sum(T_a - T_0) \Delta t \quad (1)$$

where:

M (t) = maturity (temperature-time factor) at age t, in ° C.days or ° C.hours,

Δt = time interval, in days or hours,

T_a = concrete average temperature during interval Δt , en °C, and

T_0 = reference temperature in ° C.

The reference temperature is the temperature at which ceases the strength gain of concrete; therefore, the periods during which the temperatures are at or below this temperature reference, do not contribute to resistance. Generally, a value of -10 ° C to the reference temperature in Nurse-Saul equation (325.11R ACI-01, 2001) is used.

The maturity can also be determined using the Arrhenius method, considering the nonlinearity in the rate of hydration of cement. The method Arrhenius produces a maturity index in terms of an "equivalent age", representing the equivalent time of curing, to a reference temperature, usually 20 ° C, required to produce a maturity equal to that achieved for a period of curing at temperatures other than the reference temperature, equation 2.

$$t_e = \sum e^{-Q \left(\frac{1}{T_a} - \frac{1}{T_s} \right)} \Delta t \quad (2)$$

where:

t_e = equivalent age to a reference temperature T_s , in days or hours,

Q = activation energy divided by the general gas constant, in K,

T_a = concrete average temperature during the interval Δt , in K,

T_s = reference temperature, in K and

Δt = time interval, in days or hours.

The Arrhenius equation is a better representation of the temperature-time function than the Nurse-Saul equation, when a wide variation is expected in the concrete temperature. In addition, the focus of the Nurse-Saul equation is limited according to the assumption that the rate of strength gain is a linear function. However, the Nurse-Saul formula is more widely used, primarily because of its simplicity. Both functions are considered in ASTM C 1074 (Barreda M. F., M. J. Naber, Quispe Sallo I., J. D. Sota, 2003).

Because maturity is dependent only on the history of time and temperature of the concrete, the most basic equipment requirements to determine maturity are a thermometer and a clock. However, over the years, it has developed several devices to monitor and record automatically concrete temperatures versus time. These devices connect to thermocouples embedded in the concrete and can be computed by the Nurse-Saul equation and the Arrhenius equation, at defined intervals (ASTM C 1074, 1998).

In the case of this work, we have developed a prototype measurement equipment together with software, in order to perform the experiments (Sota J. D., F. A. Avid, Chury M., P. Moreira, 2014).

2. METHODOLOGY

An equipment measurement was developed and supplemented with software that allowed to handle the data. The system design includes a series of temperature sensors connected to a microcomputer (Figure 1), which also recorded the temperature on the concrete surface. (Figure 2). The microcomputer reads the temperature of sensors and records your values. (Figure 3). A program performs a continuous reading of the information generated that is then stored in a database, enabling processing using the expressions for calculation of Nurse-Saul maturity and / or Arrhenius.



Figure 1. Microcomputer (RaspberryPi B+)



Figure 2. Digital thermometers



Figure 3. Sensors

Were studied the concrete bases of a structure in an extension of the laboratories of the Faculty, with monitoring the development of resistance to the measure of the maturity of concrete, with sensors placed in them. (Figure 4). The bases to place the sensors were chosen based on their location in the structure and the collocation steps of the concrete during the day. Which allowed have values of register in concretes placed in the morning (Base 7), averaged the concrete fill (Base 3) and end of the same (Base 10).



Figure 4. Attaching sensors

The dosage was composed of a CPC-40 portland cement, portland composite cement (up to three additions) mortar resistance of 40 MPa (IRAM 50000); thick silica sand from a quarry in the area; siliceous boulder sizes 1: 3 and 1: 2 and superplasticizer additive. The characteristics of the aggregates are reported in Table 1.

Table 1. Aggregate characteristics

Material	Fineness modulus	Maximum size	P.U. volume
Thick silica sand	2,69	--	1, 5
Boulder 1:3	7,26	1"	1, 7
Boulder 1:2	6,70	3/4"	1, 6

The proportions of the members dosing materials are summarized in Table 2.

Table 2. Dosing of concrete used in the experiences

Material	P.e (g/cm ³)	Volume (liters)	Weight (kg)
Water	1,00	158	158
Cement	3,11	101	315
Thick silica sand	2,62	309	811
Boulder 1:2	2,66	167	444
Boulder 1:3	2,67	249	666
Additive	2,5 kg. / m ³		
Air (%)	2		
Asentamiento (cm)	10		
Average resistance 28 days	25 MPa		

Were prepared 15x30 cylindrical specimens for resistance determination to different ages studied, simultaneously with the placement of concrete. So that the resistances of the specimens they corresponded to the concrete placed on the base they were sensors placed. Temperature measurements

were made on the bases 3, 7 and 10 of the structure. Strength tests were performed with a Digital Press PILOT 4 Automatic (Controls Italy) 200 tons of capacity; with real-time graphical display of test data, load curve / time and the actual load speed and simultaneous display of load, stress and actual load speed depending on loads or stresses. The tested specimens were kept in the environment of the basis on which the measurements were made during the experience, under the same conditions of humidity and temperature (25.5 to 27.5 ° C and 75% RH).

3. RESULTS

It obtained the data of resistance in compression tests of specimens and temperature with equipment designed for these experiences (located at bases 3, 7 and 10), it proceeded to correlate these to the split times used. (Details of the madurómetro and resistance at the same age).

The Nurse-Saul formula was used - Maturity (°C.h) for variables, time, temperature and strength - . Figure 5 shows the time relationship vs. maturity to the base 10 (as an example) and Figures 6, 7 and 8 the strenght relationship vs. maturity for bases 3, 7 and 10.

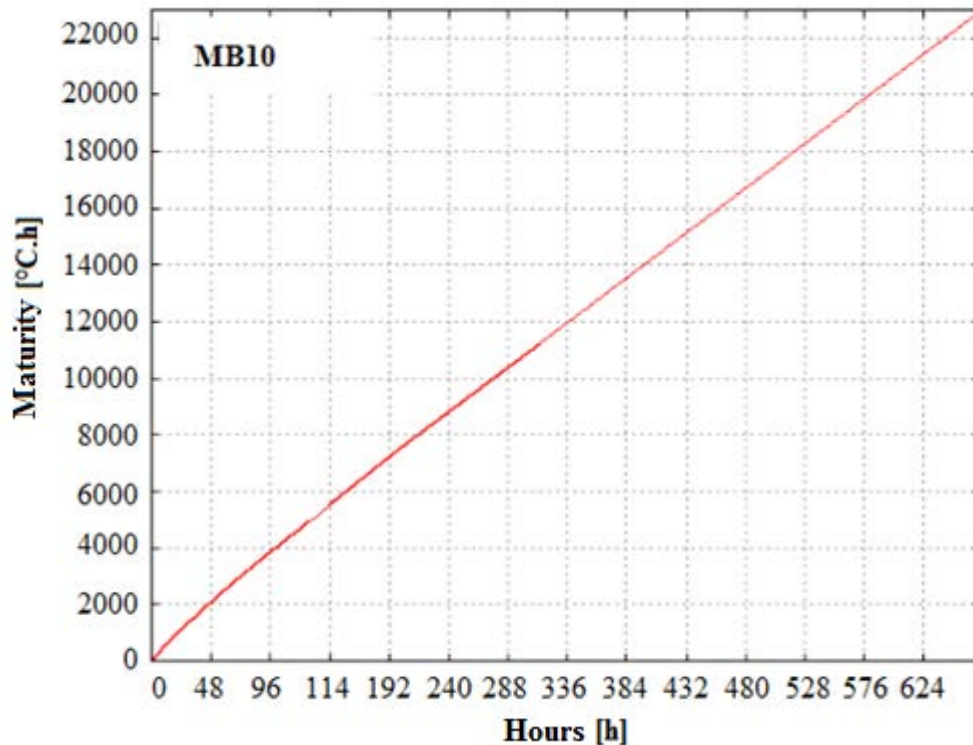


Figure 5. Time vs maturity Base 10

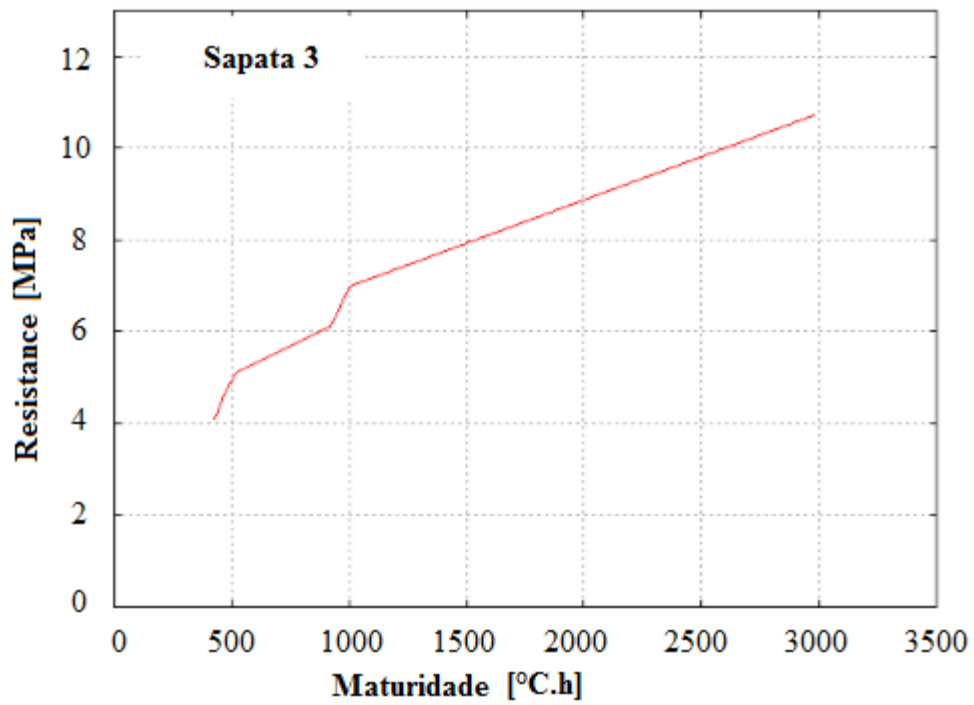


Figure 6. Resistance vs maturity Base 3

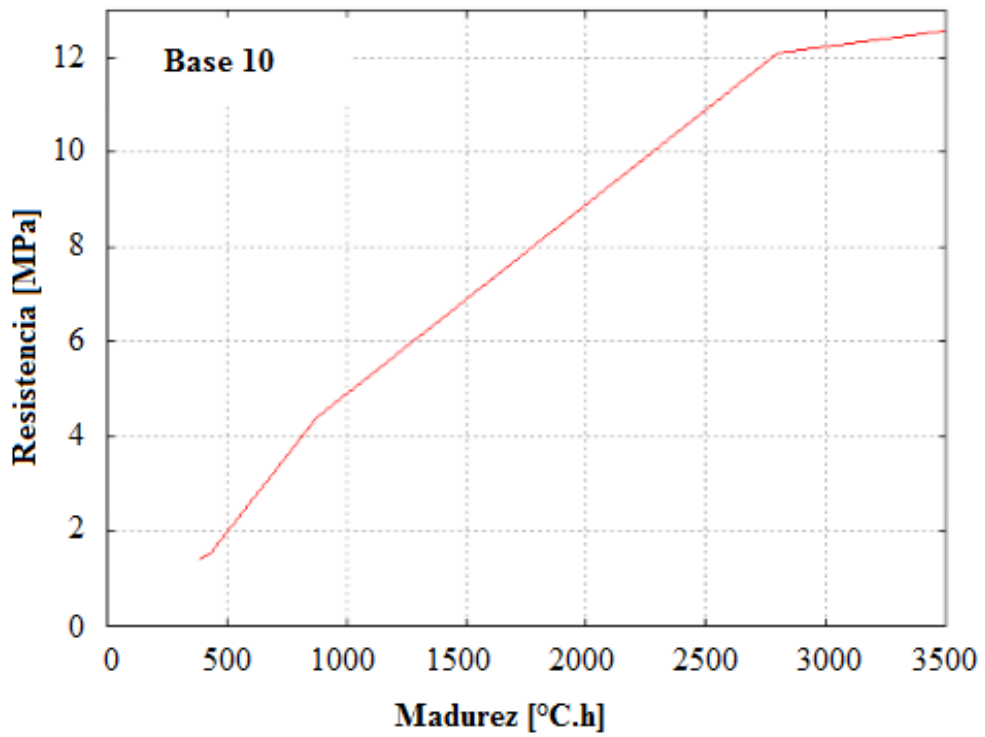


Figure 7. Resistance vs maturity Base 10

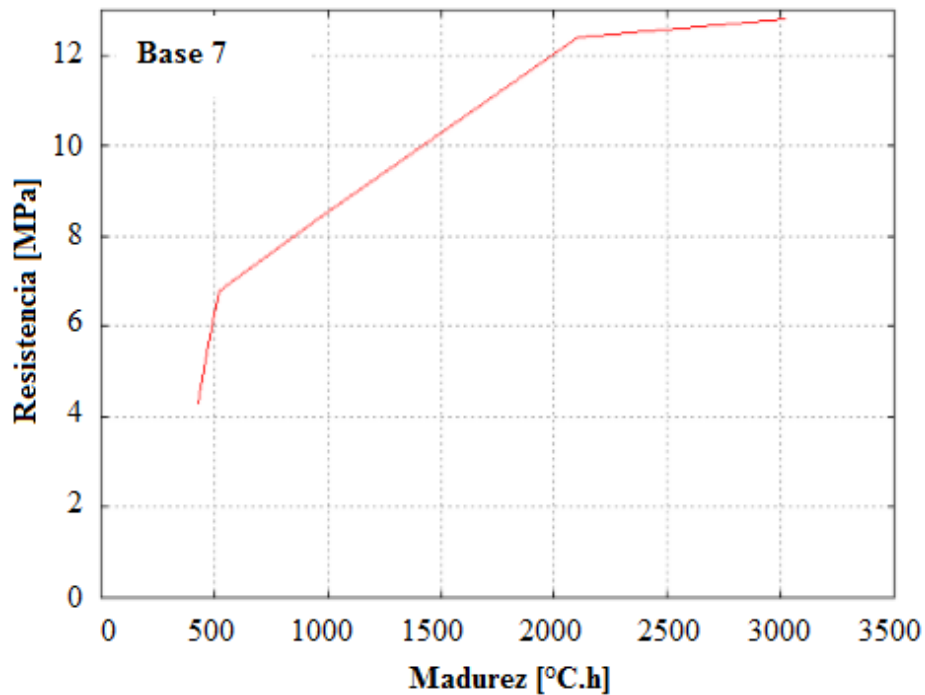


Figure 8. Resistance vs maturity Base 7

A good correlation between the measured values of maturity and corresponding resistances are observed therein. The graphics express the actual resistance values determined with each base test specimens. Table 3.

The sensors confirm that the concrete delivered to the work met the resistance value required by the specification (H21). The values at 28 days of resistance confirm this.

Table 3. Resistances certain of the bases with concrete specimens at different ages.

Base 3		Base 7		Base 10	
Age hours	Strength in MPa	Age hours	Strength in MPa	Age hours	Strength in MPa
9	1,4	--	--	--	--
10	1,5	10	4,1	10	4,0
11	--	11	4,7	11	5,6
12	--	12	5,0	12	6,8
20	4,4	20	--	20	--
21	--	21	6,1	21	--
22	--	--	--	22	8,4
23	--	23	7,0	23	--
68	12,1	73	10,7	74	12,8
667	25,0	--	--	--	--

4. FINAL CONSIDERATIONS

In function on the results, obtained of this first experience can make the following considerations: The use of this methodology allows to control the entire concrete received, without taking a significant amount of samples for further testing.

The lecture of sensors allows monitor homogeneity of the concrete and the development of resistance day to day. The methodology is applied in our next experience monitoring resistance in a complete concrete structure (slabs, beams and columns).

5. THANKS

The authors thank Dinale Construction Company S.A., the processor of concrete COINAR S.R.L. by collaboration and data provided for the experiences and the members of GIICMA Group for their collaboration in trials, particularly the students Fellows Civil Ing.; Andrea Pereyra and Alberto Palacios.

6. REFERENCES

- ACI 325.11R-01 (2001), American Concrete Institute. Accelerated Techniques for Concrete Paving.
- ASTM C 1074(1998), Standard Practice for Estimating Concrete Strength by the Maturity Method.
- Barreda, M. F., Naber, M.J., Quispe Sallo, I., Sota, J. D. (2013), “*Fisuras de contracción en pavimentos de hormigón y el aserrado de juntas*”, XII Congreso Latinoamericano de Patología de la Construcción y XIV Congreso de Control de Calidad en la Construcción. CONPAT 2013. Octubre de 2013. Cartagena de Indias, Colombia.
- Sota, J. D., Avid, F. A., Chury, M., Moreira P. (2014), “*Medida de la madurez del hormigón de pavimentos urbanos para determinar su resistencia. Diseño de equipamiento*”, X Congreso Internacional sobre Patología y Recuperación de Estructuras. CINPAR 2014. 4 al 6 de junio de 2014. Santiago, Chile.
- Taylor, P. C., Kosmatka, S. H., Voigt, G. F. et al (2007), *Integrated Materials and Construction Practices for Concrete Pavement: a State-of-the-Practice Manual*, FHWA Publication No. HIF - 07 – 004.